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FIG. 1

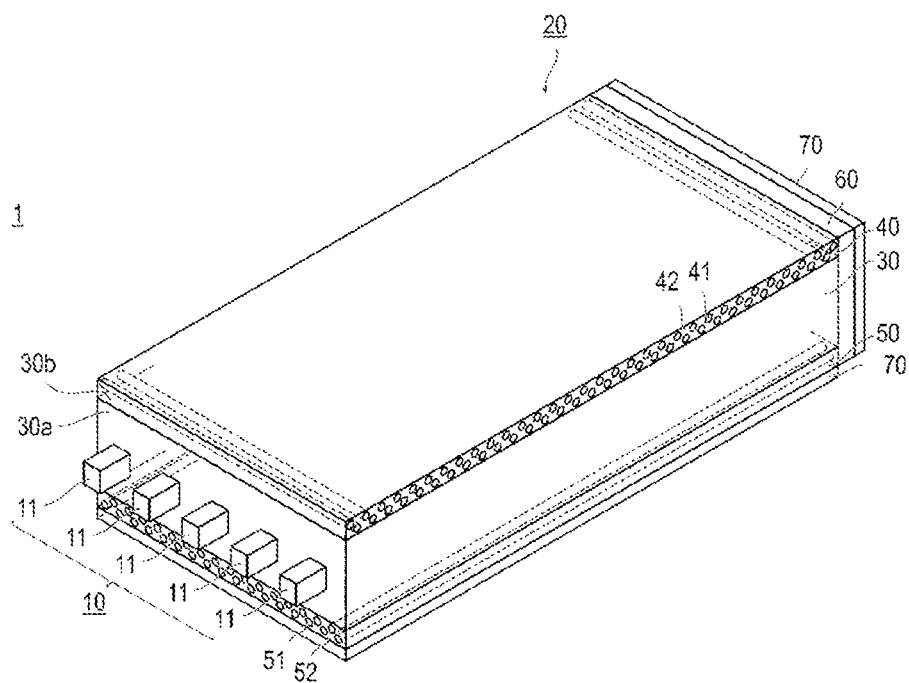


FIG. 2A

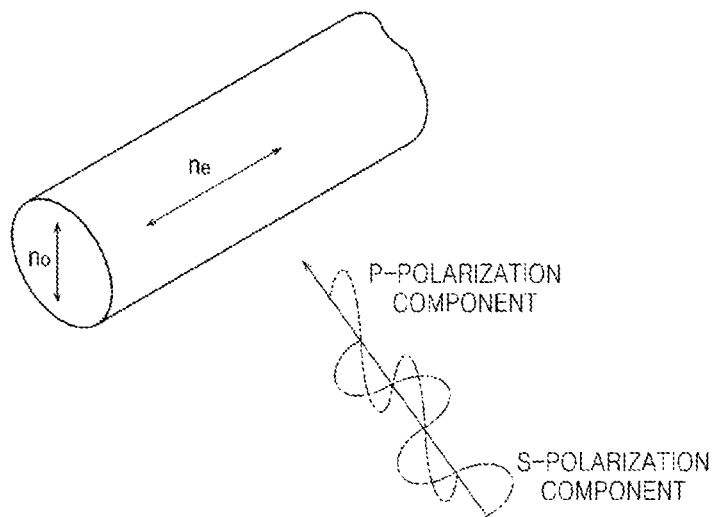


FIG. 2B

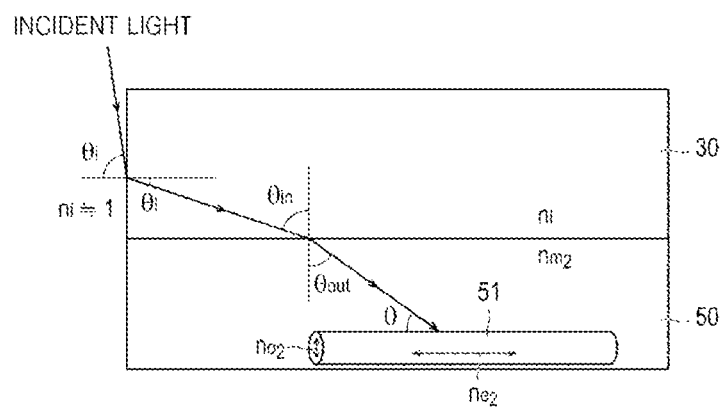


FIG. 3

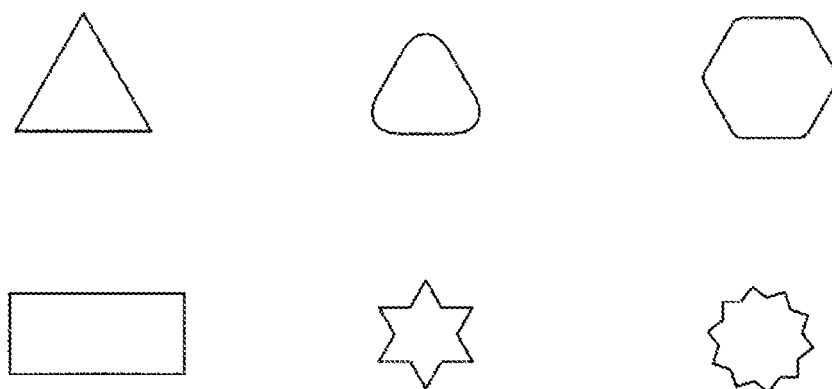


FIG. 4A

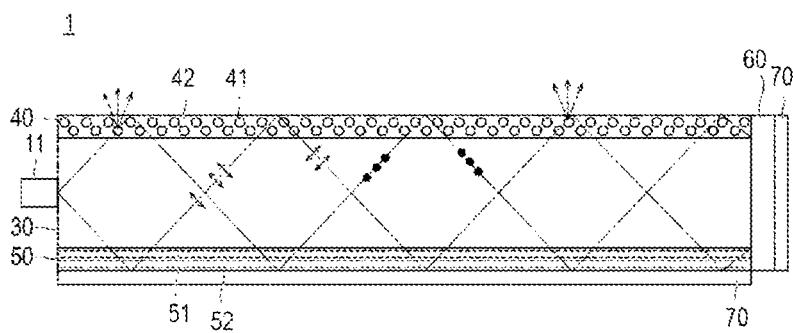


FIG. 4B

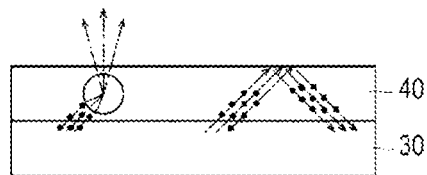


FIG. 4C

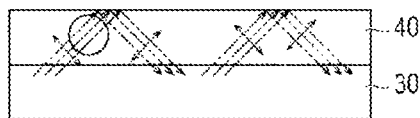


FIG. 5

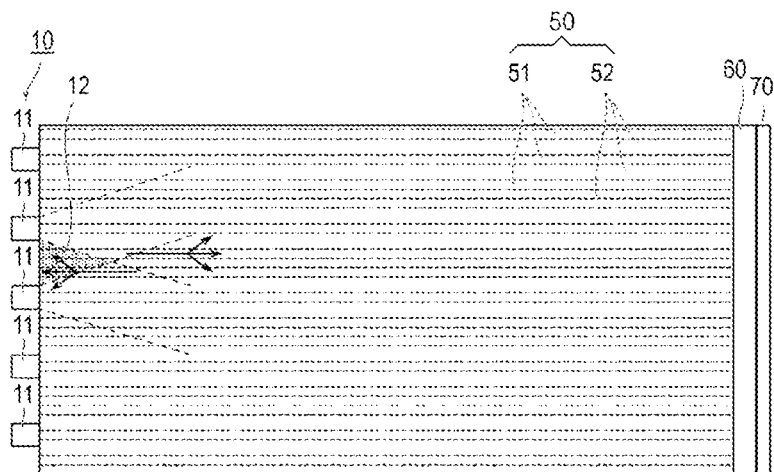


FIG. 6

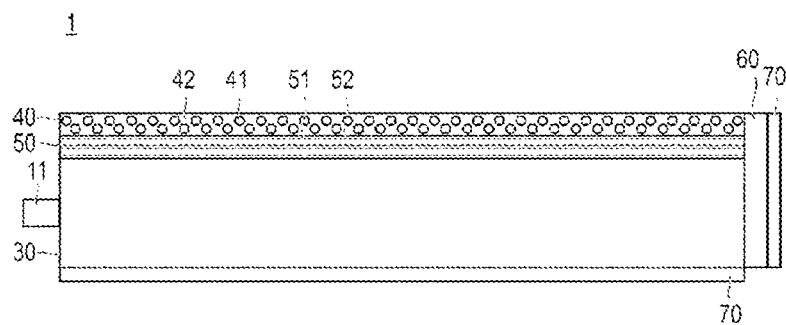


FIG. 7

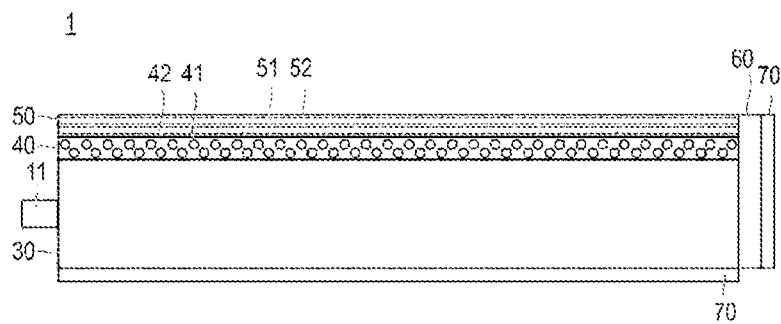


FIG. 8

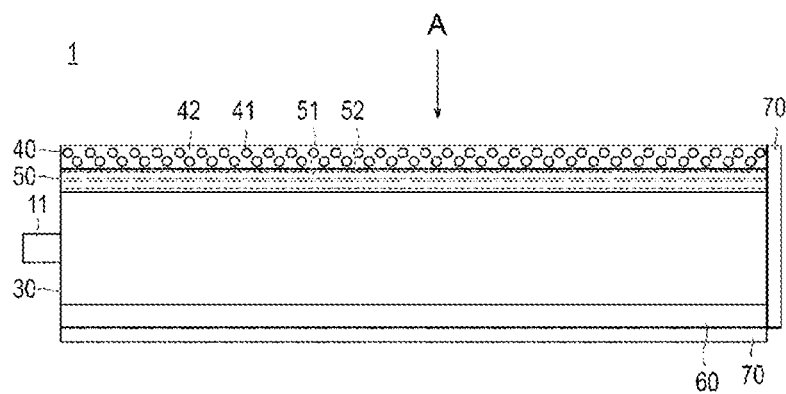


FIG. 9

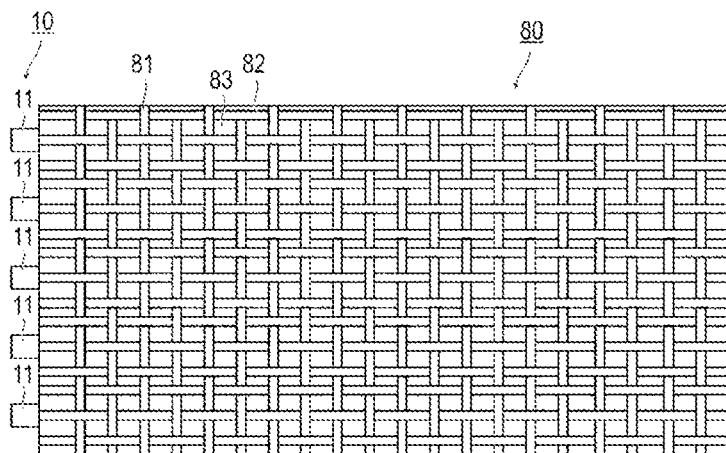


FIG. 10

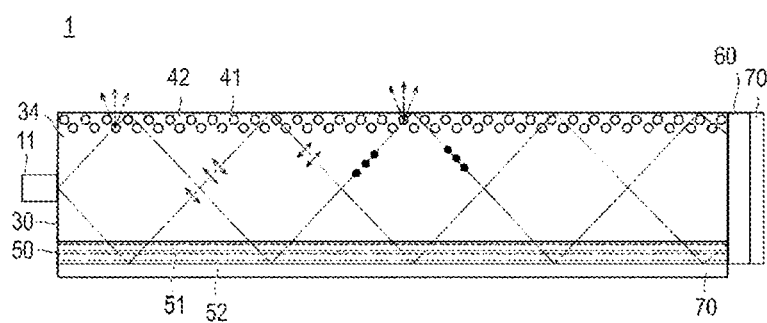


FIG. 11

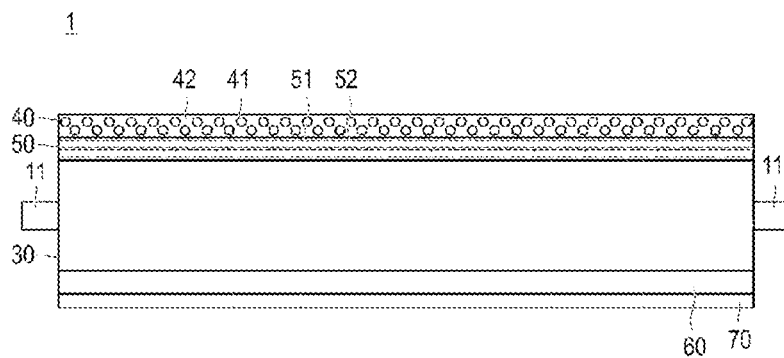


FIG. 12

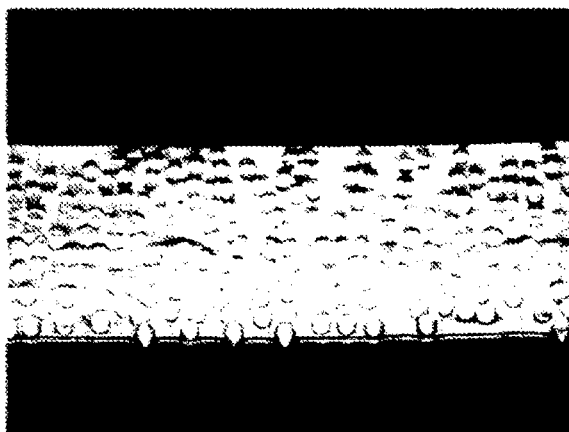


FIG. 13

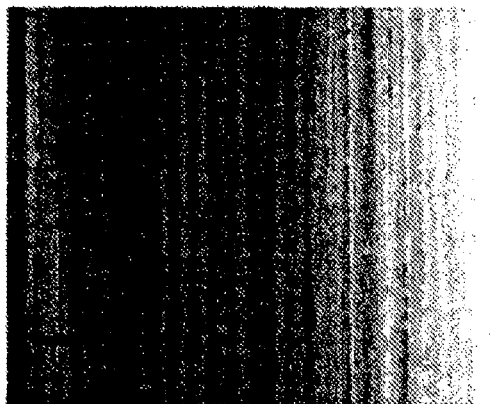
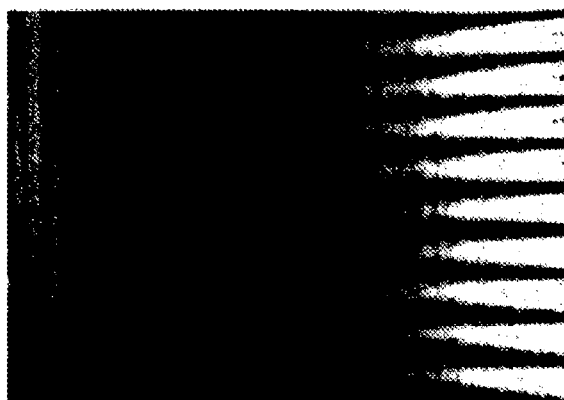


FIG. 14



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LIGHT GUIDE PANEL, SURFACE LIGHT SOURCE APPARATUS INCLUDING LIGHT GUIDE PANEL, AND FLAT PANEL DISPLAY INCLUDING SURFACE LIGHT SOURCE APPARATUS

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the benefit of Japanese Patent Application No. 2011-0140649, filed on Jun. 24, 2011, and Korean Patent Application No. 10-2012-0005277, filed Jan. 17, 2012, the disclosure of each of which is incorporated herein in its entirety by reference.

BACKGROUND

1. Field

The present disclosure relates to display apparatuses and more particularly, to light guide panels, surface light source apparatuses including the light guide panels, and/or flat panel displays including the surface light source apparatuses.

2. Description of the Related Art

Liquid crystal displays used in personal computers (PCs), computer monitors, liquid crystal display (LCD) TVs, mobile communication terminals, or the like are light-receiving displays that do not emit light by themselves but display images by selectively transmitting light irradiated from the outside. Thus, a backlight is included on a rear surface of the liquid crystal displays as a surface light source apparatus.

In the liquid crystal displays, light emitted from the surface light source apparatus transmits through a liquid crystal layer arranged between a pair of polarization plates that have transmission axes at right angles to each other. An image is displayed as the light that transmits through the liquid crystal layer is electrically turned on or off.

An absorption-type polarization plate is used as the polarization plates. In the absorption-type polarization plate, an iodine-colored uniaxially oriented polyvinyl alcohol film is used as a polarizer. A protection film such as triacetyl cellulose film or the like, and a coating layer formed of an acrylic resin, or a phase difference film such as norbornene or polycarbonate is formed on one or both sides of the polarizer.

The absorption-type polarization plate transmits only light in a direction of a transmission axis of the polarization plate and absorbs the other components of light. Thus, in principle, light usage efficiency thereof (light transmittance) does not exceed 50%. Moreover, considering that reflectivity of an inner surface of the absorption-type polarization plate is 4%, the light usage efficiency of the absorption-type polarization plate is 46% at the greatest. Thus, to achieve low power consumption by liquid crystal displays, an efficient use of the backlight and an improvement in luminance are desirable.

As one of the methods for solving the above-described problem, a reflective polarization plate that uses optical reflection and interference is known. The reflective polarization plate reflects a desired polarization component light and transmits polarization of the opposite property to the desired polarization component light.

An axis of the reflective polarization plate is adjusted such that only polarization in a transmission axis direction is transmitted so that the light transmitted through the reflective polarization plate remains the same as linear polarization, and at the same time, the absorbed polarization is reflected for reuse in the absorption-type polarization plate. Thus, light usage efficiency of light emitted from the backlight may be improved.

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An example of the reflective polarization plate is a dual brightness enhancement film (DBEF) including refractive index isotropic layers and refractive index anisotropic layers that are alternately stacked. However, a DBEF requires polymer films of several hundreds of stacked layers in total in order to provide polarization over a visible region. Thus, precise control is needed and this increases manufacturing costs.

To improve light usage efficiency and polarization separation power more cost-effectively, a technique of using a polarization sensitive scattering element (PSSE) is being researched. For example, Prior Art 1 (Japanese Patent Publication No. Hei 11-502036) discloses a method in which a polarization component in a direction perpendicular to a transmission axis is scattered to the backside by using a PSSE, and a polarization state of a corresponding backside scattering component is converted by using a series of stacked layers.

In addition, Prior Art 2 (Japanese Patent Publication No. 2009-047802) discloses a reflective polarization plate in which a birefringent body formed of fibers having birefringence is used as a PSSE. In the reflective polarization plate, a layer in which a refractive index in a cross-sectional direction of the birefringent body (ordinary ray refractive index) corresponds to a refractive index of a supporting medium (polarization layer A) and a layer (polarization layer B) in which a refractive index in a length direction of the birefringent body (ordinary ray refractive index) corresponds to a refractive index of a supporting medium are alternately stacked such that arrangement directions of the birefringent bodies cross each other. Accordingly, polarization separation with respect to light that is obliquely incident or diffused light is improved.

In addition, Prior Art 3 (Japanese Patent Publication No. 2006-517720) discloses a method of improving polarization separation efficiency by scattering only one component of polarization and emitting the same to the outside by integrating an isotropic resin layer, in which birefringence fibers are buried as a PSSE, into a light guide panel.

To reduce power consumption of the surface light source apparatuses, LEDs having a long life span and power consumption reduction effect are frequently used as a backlight.

SUMMARY

At least one example embodiment including light guide panels for improving polarization separation efficiency and preventing luminance spots even when a discontinuous light source is disposed on a cross-section of the light guide panels is provided.

At least one example embodiment including surface light source apparatuses including the light guide panels is provided.

At least one example embodiment including flat panel displays including the surface light source apparatuses as a light source apparatus is provided.

Additional example embodiments will be set forth in part in the description that follows and, in part, will be apparent from the description, or may be learned by practice of the presented example embodiments.

According to an example embodiment, a light guide panel includes: a light guide layer including a light incident surface; a polarization separation layer configured to select a desired polarization among light emitted from the light guide layer and to emit light having the polarization; and a light homogenization layer including a plurality of first fibers and a first supporting medium of the first fibers, the light homogeniza-

tion layer configured to diffuse and scatter light incident on the light guide layer into the light guide layer.

The polarization separation layer may include: a plurality of second fibers having birefringence; and a second supporting medium that is isotropic and configured to support the second fibers.

A refractive index of the second supporting medium may correspond to at least one of two different refractive indices of the second fibers.

The plurality of first fibers have birefringence and the first supporting medium is isotropic and configured to support the first fibers.

A refractive index of the first supporting medium may be different from at least one of the two different refractive indices of the first fibers.

A surface roughness R_z of an outer circumferential surface of the second fibers may be from about $0.1\text{ }\mu\text{m}$ to about $10\text{ }\mu\text{m}$.

The second fibers may have a polygonal cross-section in a radius direction.

One of the light guide layer, the polarization separation layer, and the light homogenization layer may be between the remaining two layers.

The light guide panel may further include: a phase difference plate configured to convert a polarization direction of light in the light guide layer; and a reflection plate on a surface except the light incident surface and a light emitting surface of the light guide layer, the reflection plate configured to reflect light emitted from the light guide layer back into the light guide layer.

The polarization separation layer and the light homogenization layer may be stacked on the light emitting surface of the light guide layer. The polarization separation layer and the light homogenization layer may be integrated into a single layer. In the single layer, the first fibers and the second fibers may alternate, and a third supporting medium may include the first and second supporting media that supports the first and second fibers.

The first fibers and the second fibers may be different materials.

The light guide layer may be a same material as at least one of the first and second supporting media.

A density of the second fibers may be higher away from the light incident surface.

A density of the first fibers may vary according to arrangement positions.

Some of the plurality of first and second fibers may include discontinuous portions.

Portions of the plurality of first and second fibers may be overlapped.

According to another example embodiment, a surface light source apparatus including: a light source unit including a plurality of light sources spaced apart from one another; and a light guide panel configured to emit light having a polarization component of light incident from the light source unit, wherein the light guide panel is one described above.

A density of the first fibers may be higher between the plurality of light sources.

The plurality of light sources may be on two opposite sides of the light guide panel.

According to another example embodiment, a flat panel display includes: a light source apparatus; and a liquid crystal panel configured to display an image by using light supplied from the light source apparatus, wherein the light source apparatus is the surface light source apparatus described above.

According to some example embodiments, light is scattered and diffused at various angles in an in-plane direction

via a light homogenization layer in which first fibers extended vertically to an incident surface are arranged. Thus, even when a discontinuous light source is used, uniform luminance may be obtained.

By using a polarization separation layer in which second fibers extended parallel to an incident surface are arranged, only desired polarization components may be selectively emitted with a high polarization separation efficiency.

BRIEF DESCRIPTION OF THE DRAWINGS

These and/or other aspects will become apparent and more readily appreciated from the following description of the example embodiments, taken in conjunction with the accompanying drawings in which:

FIG. 1 is a perspective view of a surface light source apparatus according to an example embodiment;

FIGS. 2A and 2B are schematic views illustrating an example of a relationship between a fiber and a refractive index;

FIG. 3 is a cross-sectional view illustrating a modified example of a cross-section of the fiber shown in FIG. 2A;

FIG. 4A is a right-side cross-sectional view illustrating the surface light source apparatus of FIG. 1;

FIG. 4B is an expanded view of FIG. 4A illustrating propagation of an S-polarization component incident to a polarization separation layer;

FIG. 4C is an expanded view of FIG. 4A illustrating propagation of a P-polarization component incident to the polarization separation layer;

FIG. 5 is a bottom view of the surface light source apparatus of FIG. 1;

FIG. 6 is a side view of a surface light source apparatus according to another example embodiment;

FIG. 7 is a side view of a surface light source apparatus according to another example embodiment;

FIG. 8 is a side view of a surface light source apparatus according to another example embodiment;

FIG. 9 is a side view of a surface light source apparatus according to another example embodiment;

FIG. 10 is a side view of a surface light source apparatus according to another example embodiment;

FIG. 11 is a side view of a surface light source apparatus according to another example embodiment;

FIG. 12 is an image of a cross-section of a polarization separation layer formed in a surface light source apparatus according to another example embodiment;

FIG. 13 is an image illustrating two-dimensional luminance distribution of light emitted through an image plane of a light guide panel (light-emitting surface) of a surface light source apparatus according to another example embodiment; and

FIG. 14 is an image illustrating two-dimensional luminance distribution of light emitted through an image plane of a light guide panel (light-emitting surface) of a surface light source apparatus according to a comparative example.

DETAILED DESCRIPTION

Reference will now be made in detail to example embodiments, examples of which are illustrated in the accompanying drawings, wherein like reference numerals refer to like elements throughout. In this specification, thicknesses of layers or regions illustrated in the drawings are exaggerated for clarity of description. In addition, measurement ratios in the drawings are exaggerated for convenience of description and may vary from actual ratios. In this regard, the example embodiments may have different forms and should not be

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construed as being limited to the descriptions set forth herein. Accordingly, the example embodiments are merely described below, by referring to the figures, to explain aspects of the present description. As used herein, the term “and/or” includes any and all combinations of one or more of the associated listed items. Expressions such as “at least one of,” when preceding a list of elements, modify the entire list of elements and do not modify the individual elements of the list.

When a (e.g., layer, region, or plate) is referred to as being herein “on,” “connected to,” or “coupled to” another member, the member may be directly on, or connected or coupled to the another member or intervening member(s) between the member and the another member may be present.

A surface light source apparatus according to some example embodiments will be described.

FIG. 1 is a perspective view of a surface light source apparatus 1 according to an example embodiment.

FIGS. 2A and 2B are schematic views illustrating an example of a relationship between a fiber and a refractive index, and FIG. 3 is a cross-sectional view illustrating a modified example of a cross-section of the fiber.

As illustrated in FIG. 1, the surface light source apparatus 1 is an edge light type surface light source apparatus. The surface light source apparatus 1 includes a light source unit 10 and a light guide panel 20 transmitting a desired polarization component among the light emitted from a plurality of light sources 11 of the light source unit 10. In an example embodiment, light is emitted as surface emission from the surface light source apparatus 1 in an upward direction of FIG. 1. Although not shown in FIG. 1, when the surface light source apparatus 1 is applied to a liquid crystal display, a liquid crystal unit may be arranged on a surface of the surface light source apparatus 1 from which light is emitted.

The light source unit 10 emits light to be supplied in the surface light source apparatus 1 and the light source unit 10 is on a side of the light guide panel 20. The light source unit 10 includes a plurality of light sources 11 arranged at intervals. The intervals between the plurality of light sources 10 may be regular or irregular.

While the plurality of light sources 11 are arranged one-dimensionally in FIG. 1, they may also be arranged two-dimensionally. For example, the plurality of light sources 11 may be point light-emitting diodes (LEDs).

The light guide panel 20 may include a rectangular parallelepiped plate. The light guide panel 20 includes a light guide layer 30, a polarization separation layer 40 stacked on the light guide layer 30, a light homogenization layer 50 stacked on the light guide layer 30, and a phase difference plate 60 and a reflection plate 70 on the light guide layer 30. The polarization separation layer 40 and the light homogenization layer 50 face each other with the light guide layer 30 interposed therebetween. The light guide layer 30 allows light emitted from the light source 11 to be incident to an incident surface 30a, which is a side surface thereof, and enter the light guide panel 20. The entered light is propagated in the light guide layer 30 and only a desired polarization component is selectively emitted from the polarization separation layer 40. The light guide layer 30 may be formed of a transparent material capable of transmitting incident light. The transparent material may be, for example, an optical isotropic material such as polymethyl methacrylate (PMMA) or polycarbonate (PC). The polarization separation layer 40 is stacked on the light guide layer 30. The polarization separation layer 40 derives desired polarization among the light in the light guide layer 30 from a light emitting surface 30b of the light guide layer 30, which is a principal surface of the light guide layer 30 on a side. The polarization separation layer 40 reflects polarization light that

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is perpendicular to this derived polarization. The polarization separation layer 40 may be on an outer surface of the light guide layer 30 but is not limited thereto.

The polarization separation layer 40 may include a first fiber 41 and a first supporting medium 42 that supports the first fiber 41. For example, the first fiber 41 may extend parallel to the incident surface 30a of the light guide layer 30, or may extend in a direction which is inclined by about $\pm 45^\circ$ with respect to the direction parallel to the incident surface 30a. The first fiber 41 may be provided in plural. That is, the polarization separation layer 40 may include a plurality of first fibers 41. The light homogenization layer 50 is stacked on the light guide layer 30. The light homogenization layer 50 homogenizes a light direction by diffusing light in the light guide layer 30 in an in-plane direction, for example, in a direction perpendicular to a light propagation direction. The light homogenization layer 50 includes a second fiber 51 and a second supporting medium 52 that supports the second fiber 51. For example, the second fiber 51 may extend in a direction perpendicular to the incident surface 30a of the light guide layer 30, or may extend in a direction which is inclined by about $\pm 45^\circ$ with respect to the direction perpendicular to the incident surface 30a.

The light homogenization layer 50 includes a plurality of second fibers 51. The plurality of second fibers 51 are parallel to the incident surface 30a of the light guide layer 30. For example, the second fibers 51 are arranged in a direction perpendicular to the arrangement direction of the first fibers 41 of the polarization separation layer 40. The first and second fibers 41 and 51 of the polarization separation layer 40 and the light homogenization layer 50 have birefringence. The first and second fibers 41 and 51 have an extraordinary ray refractive index n_e and an ordinary ray refractive index n_o . The refractive index n_e is greater than the refractive index n_o .

The relationship between refractive indices of the first and second fibers 41 and 51 will be described below with reference to FIGS. 2A and 2B.

As illustrated in FIGS. 2A and 2B, the first and second fibers 41 and 51 have the ordinary ray refractive index n_o in a cross-sectional direction that is smaller than the extraordinary ray refractive index n_e in a length direction. The first and second fibers 41 and 51 may be formed of various materials having birefringence. For example, a polymer fiber that is prepared by extending a polymer may be used for a stable cross-section, excellent durability, and easy orientation characteristics.

Examples of the polymer fiber may include polyolefin fibers such as polyethylene (PE), polytetrafluoroethylene (PTFE), polypropylene (PP); polyvinyl fibers such as polyfluorinated vinylidene (PVdF), polyfluorinated vinyl (PVF), polyvinyl chloride (PVC), or polyvinyl alcohol; and acrylic fibers such as polyacrylonitrile (PAN).

The polymer fiber may be aliphatic polyamide fiber such as Nylon 6 (N6), Nylon 6,6 (N66), Nylon 4,6 (N46), or Nylon 6,10 (N610); aromatic polyamide fibers (aramid fiber) such as poly(m-phenyleneisophthalamide) (PMPiA) or poly(p-phenylene terephthalamide) (PMPTA); or polyester fibers such as polyethylene terephthalate (PET), polyethylene naphthalate (PEN), or poly-ε-caprolactone.

The polymer fiber may be animal fibers such as silk, wool, or cobweb, or cellulose vegetable fiber such as cupra, rayon fibers, etc. The types of the first fiber 41 and the second fiber 51 may be selected to satisfy the relationship between refractive indices that will be described below, or the same or different types may be used. Various types of fibers may be used in the polarization separation layer 40 or the light homogenization layer 50.

The first and second fibers **41** and **51** may be formed of a polymer fiber. This polymer has a great refractive index difference Δn between an extraordinary ray refractive index n_e and an ordinary ray refractive index n_o . The larger the refractive index difference Δn is, the more improved polarization separation efficiency of the polarization separation layer **40** or light diffusion efficiency of the light homogenization layer **50** may be. The difference Δn in the refractive indices may be 0.03 or greater, and for example, 0.05 or greater or 0.1 or greater.

The extraordinary ray refractive index n_e and the ordinary ray refractive index n_o of the polymer fiber may be controlled by adjusting a tensioning speed of a polymer, or a tensioning rate thereof, a material of the polymer, a thickness (diameter) or density of a fiber.

Table 1 below shows an extraordinary ray refractive index n_e and an ordinary ray refractive index n_o of representative draft polymer fibers. The refractive indices of Table 1 are calculated by dipping a fiber in liquids of various refractive indices, adjusting a liquid that is invisible as fiber lines are assimilated with the liquid by using a polarization microscope, and measuring the refractive index of the adjusted liquid using Atagosa Digital Abbe Refraction System DRA1 (wavelength: 589 nm). The refractive index of the adjusted liquid may be measured with respect to each of transmission axes of polarization to measure n_o and n_e .

TABLE 1

Ordinary ray refractive index n_o and extraordinary ray refractive index n_e of representative polymer fibers					
Material	Abbreviation	Thickness (μm)	n_o	n_e	Δn
Nylon 6	N6	75	1.5182	1.6228	0.1046
Nylon 6	N6	90	1.5182	1.6104	0.0922
Nylon 6,10	N610	50	1.5217	1.5711	0.0494
Nylon 6,10	N610	100	1.5217	1.5711	0.0494
Nylon 6,6	N66	100	1.5182	1.5971	0.0789
Polyfluorinated vinylidene	PVdF	70	1.4193	1.4501	0.0308
Polyethylene terephthalate	PET	16	1.5449	1.7200	0.1751

Thicknesses of the first and second fibers **41** and **51** may vary. The thicknesses of the first and second fibers **41** and **51** may be controlled according to a size of a display to which they are applied. The thicknesses of the first and second fibers **41** and **51** may be controlled to have desired refractive indices. For example, the thicknesses of the first and second fibers **41** and **51** may be from about 1 μm to about 200 μm .

The intervals between the first and second fibers **41** and **51** may vary. The intervals between the first and second fibers **41** and **51** may be selected according to a size of a display and to be smaller than a pixel pitch of a liquid crystal display to which the first and second fibers **41** and **51** are applied. The intervals between the first and second fibers **41** and **51** may be regular or irregular. The first and second fibers **41** and **51** may have a single-layer structure or a multi-layer structure.

The first fibers **41** may be arranged with uniform or non-uniform density. For example, the first fibers **41** may be arranged with a density that increases away from the light sources **11**. For example, a density of the first fibers **41** in the polarization separation layer **40** may increase continuously or stepwise away from the light sources **11**. A light amount is reduced away from the light sources **11**. Accordingly, in an area with a small light amount and away from the light sources **11**, the first fibers **41** may be densely arranged. In an

area with a large light amount near the light sources **11**, the first fibers **41** may be coarsely arranged. Accordingly, a uniform light may be emitted over the entire image plane (light-emitting surface) of the light guide panel **20**.

Lengths of the first and second fibers **41** and **51** may be determined according to a size of the polarization separation layer **40** or a size of the light homogenization layer **50** in which the first and second fibers **41** and **51** are arranged. The lengths of the first and second fibers **41** and **51** are not limited to being continuous in a longitudinal direction of the polarization separation layer **40** or the light homogenization layer **50**. For example, some portions of the first and second fibers **41** and **51** may be removed and discontinuous portions may be present. Some of the first and second fibers **41** and **51** may be overlapped. The first and second fibers **41** and **51** may have a circular cross-section as illustrated in FIG. 1 but are not limited thereto, and may have a different cross-section. For example, as illustrated in FIG. 3, the first and second fibers **41** and **51** may have a regular or irregular polygonal cross-section such as a triangular, rectangular, or hexagonal cross-section, or a cross-section formed by combining a curved line and a straight line. "Polygonal cross-section" includes not only figures respective sides of which formed by straight lines, but also figures respective sides of which are formed by curved lines. For example, polygonal cross-sections of the first and second fibers **41** and **51** may have some curved lines on each side or on each vertex, and these cross-sections are also included in the above-described "polygonal cross-section."

As will be described below, in the polarization separation layer **40**, only a desired polarization component of light is selectively scattered by the first fibers **41**, and emitted from the light emitting surface **30b**. The light is likely to scatter in a light guide direction, and thus, the amount of scattered light in a direction perpendicular to a light proceeding direction is reduced.

When a surface light source apparatus including a light guide panel according to an example embodiment is used as a backlight of a liquid crystal display, and if the first fibers **41** have a polygonal cross-section, various scattering angles are formed, and thus scattering of light may increase in a direction perpendicular to the light guide direction. As a result, light with a more uniform angle distribution may be obtained.

Forms of external circumferential surfaces of the first and second fibers **41** and **51** may vary. Surface roughness R_z of an outer circumferential surface of the first fibers **41** may be from about 0.1 μm to about 10 μm . Various light scattering angles are formed by the first fibers **41**, and thus, light with a more uniform angle distribution may be obtained. The e, tlight scattering angles are formed by the first fibers **41**, and thus, lined based on JIS B 0601-2001.

The first and second supporting media **42** and **52** support the first and second fibers **41** and **51**, respectively, and may be formed of an optically isotropic material. Accordingly, the first and second supporting media **42** and **52** may be formed of any material that has excellent adhesiveness with respect to the first and second fibers **41** and **51** and optical transparency. For example, the first and second supporting media **42** and **52** may be formed of a curable resin that is polymerable/linkable by heat or radiation.

The curable resin may be, for example, a UV-curing resin formed of a compound including, for example, an acryloyl group, a methacryloyl group, a vinyl group, an aryl group, a styryl group, a thiol group, an epoxy group, a vinyl ether group, or an oxetanyl group.

The curable resin may be a thermosetting resin formed of silicon resin, aryl ester, acrylic resin, epoxy resin, polyimide, or urethane resin.

The curable resin may be a compound of the UV-curing resin and the thermosetting resin.

The first and second supporting media **42** and **52** may be formed of an acrylic resin such as PMMA; a polyolefin resin such as PE, PP, or cycloolefin polymer (COP); a polyester resin such as PET; a polyether such as polyphenylene oxide (PPO); a vinyl resin such as polyvinyl alcohol; polystyrene, PC, polyurethane, polyamide, polyimide, or epoxy resin; a copolymer including at least two types of monomers forming these materials; or a blend of these polymers.

By mixing a plurality of resins, refractive indices (nm) of the first and second supporting media **42** and **52** may be controlled as desired.

The polarization separation layer **40** may be formed such that a refractive index nm1 of the first supporting medium **42** matches an ordinary ray refractive index no1 or an extraordinary ray refractive index ne1 of the first fiber **41**.

An example embodiment in which the refractive index nm1 of the first supporting medium **42** and the ordinary ray refractive index no1 of the first fiber **41** match each other will be described.

In this specification, "the refractive indexes nA and nB match each other" means that the refractive indexes nA and nB match each other with a precision to the second decimal point or greater, and this may also indicate that the refractive indexes nA and nB match each other with a precision to the third decimal point or greater.

The light homogenization layer **50** may be formed such that a refractive index nm2 of the second supporting medium **52** is different from at least one of an ordinary ray refractive index no2 and an extraordinary ray refractive index ne2 of the second fiber **51**.

An example embodiment in which the refractive index nm2 of the second supporting medium **52** is different from both the ordinary ray refractive index no2 and the extraordinary ray refractive index ne2 of the second fiber **51** will be described.

A phase difference plate **60** is opposite to the incident surface **30a** of the light guide layer **30**, and converts a polarization direction of light propagating in the light guide layer **30**. The phase difference plate **60** may be, for example, a $\lambda/4$ plate that shifts a phase by $\lambda/4$. The phase difference plate **60** may be included selectively. Thus, the phase difference plate **60** may also be omitted.

The reflection plate **70** prevents light in the light guide layer **30** from leaking to other portions except through the light emitting surface **30b**. To this end, the reflection plate **70** is stacked on a side except the incident surface **30a** of the light guide layer **30** or on a principal surface of the light guide layer **30** that is opposite to the light emitting surface **30b**. The reflection plate **70** is stacked on the phase difference plate **60** or the light homogenization layer **50**. Although not shown in the drawings, the reflection plate **70** may also be formed on two surfaces besides the incident surface **30a** of the light guide layer **30** and the opposite surface to the incident surface **30a**. Also, although not shown in the drawings, the reflection plate **70** may be disposed between the plurality of light sources **11** or on or under the light sources **11**.

The principle of surface emission of light from a light source in the surface light source apparatus **1** will be described.

FIG. 4A is a right-side cross-sectional view illustrating the surface light source apparatus **1** of FIG. 1. FIG. 4B is an expanded view of FIG. 4A illustrating an example of propa-

gation of an S-polarization component incident to the polarization separation layer **40**. FIG. 4C is an expanded view of FIG. 4A illustrating an example of propagation of a P-polarization component incident to the polarization separation layer **40**.

As illustrated in FIG. 4A, light is incident from the light source **11** on the incident surface **30a** of the light guide layer **30**. The incident light propagates through the light guide layer **30** by repetitive internal reflection on interfaces between the polarization separation layer **40**, the light homogenization layer **50**, and the phase difference plate **60** as denoted by a chain line or a long-and-short broken line. Light is reflected by the reflection plate **70** that is attached outside the phase difference plate **60**, below the light homogenization layer **50**, and on a side of the light guide layer **30**, and thus, is not leaked except through the light emitting surface **30b** but is propagated further in the light guide layer **30**.

Light emitted from the light source **11** is natural light, and various polarization components are mixed in the light. Hereinafter, the chain line with black circles in FIGS. 4A through 4C denotes a P-polarization component that vibrates on a plane such as a ground surface. The long-and-short broken line with arrows denotes an S-polarization component that vibrates on the plane perpendicular to the ground surface. The S-polarization component is selectively emitted from the light emitting surface **30b** by the polarization separation layer **40**.

As described above, the polarization separation layer **40** includes the first fibers **41**. As illustrated in FIG. 2A, the first fibers **41** have an extraordinary ray refractive index ne1 in a length direction and an ordinary ray refractive index no1 in a cross-sectional direction. The S-polarization component vibrates on a plane that is parallel to a cross-section of the first fibers **41** along the length direction. Accordingly, the S-polarization component may be affected by the extraordinary ray refractive index ne1 in the length direction of the first fibers **41**, but not by the ordinary ray refractive index no1 in the cross-sectional direction.

On the other hand, as the P-polarization component vibrates on a plane parallel to the cross-section of the first fibers **41**, it may be affected by the ordinary ray refractive index no1 of the first fibers **41** in the cross-sectional direction. However, the P-polarization component is not affected by the extraordinary ray refractive index ne1 of the first fibers **41** in the length direction.

The first supporting medium **42** that supports the first fibers **41** is formed to correspond to the refractive index of the first fibers **41**. Accordingly, when light is incident from the first supporting medium **42** to the first fibers **41** or from the first fibers **41** to the first supporting medium **42**, a P-polarization component propagates in a material of the same refractive index. Accordingly, the P-polarization component of light proceeds straight without being affected by the refractive index. In other words, the P-polarization component of light may propagate inside the first supporting medium, **42** in the same manner as when the first fibers **41** are not included. Accordingly, the P-polarization component denoted by the chain line of FIG. 4 is not refracted by the first fibers **41**, and thus, is reflected under an internal total reflection condition of the first supporting medium **42**.

On the other hand, the first supporting medium **42** has a refractive index that is different from the refractive index of the first fibers **41**. Accordingly, when light is incident from the first supporting medium **42** to the first fibers **41** or from the first fibers **41** to the first supporting medium **42**, the S-polarization component propagates in a material of a different refractive index. Accordingly, the S-polarization component

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is affected by the refractive index and is refracted or reflected. The S-polarization component denoted by the long-and-short broken line of FIG. 4 is refracted or reflected by the first fibers 41 and a portion thereof deviates from an internal total reflection condition of the first supporting medium 42 and is incident on an interface at an acute angle and is emitted from the first supporting medium 42.

By stacking the polarization separation layer 40 on the light guide layer 30, only an S-polarization component may be selectively scattered and be emitted from the light emitting surface 30b. As a result, a polarization component that is necessary for a liquid crystal unit may be selectively emitted.

Above is described the first supporting medium 42 having a refractive index nm1 that corresponds to the ordinary ray refractive index no1 of the first fibers 41 and that is different from the extraordinary ray refractive index ne1 of the first fibers 41.

However, the refractive index nm1 of the first supporting medium 42 may be formed to correspond to the extraordinary ray refractive index ne1 and to the ordinary ray refractive index no1 of the first fibers 41. In this case, only a P-polarization component may be selectively scattered to be emitted from the light emitting surface 30b. However, scattering efficiency may be improved when using an S-polarization component that does not vibrate within the same plane as the light guide direction of light instead of using a P-polarization component that vibrates in the same plane of the light guide direction of light. Accordingly, the refractive index nm1 of the first supporting medium 42 may be set to correspond to the ordinary ray refractive index no1 of the first fibers 41.

The principle of diffusing light in the light guide layer 30 in an in-plane direction by using the light homogenization layer 50 will be described below. FIG. 5 is a bottom view of the surface light source apparatus 1 of FIG. 1.

As illustrated in FIG. 5, the light sources 11 formed of LEDs emit light as a point light source. Thus, a light amount between adjacent light sources 11 may be reduced and dark portions may be generated in an area 12 near the light sources 11. As light propagating in the light guide layer 30 is scattered in the in-plane direction, light direction distribution in the light guide layer 30 may be homogenized. Accordingly, some of the dark portions may disappear.

The light homogenization layer 50 includes the second fibers 51 as described above. The second fibers 51 include an extraordinary ray refractive index ne₂ in a length direction and an ordinary ray refractive index no₂ in a cross-sectional direction. The second fibers 51 are arranged such that a length direction thereof corresponds to a light guide direction of light. Accordingly, light incident on the second fibers 51 is influenced by the ordinary ray refractive index no1 and the effective extraordinary ray refractive index ne_{2_eff}.

As illustrated in FIG. 2B, when light that is guided in the length direction of the second fibers 51 in the light homogenization layer 50 is incident to the second fibers 51 at an incident angle θ , the effective extraordinary ray refractive index ne_{2_eff} may be expressed as Equation (A):

$$ne_{2_eff} = \frac{ne_2 \cdot no_2}{\sqrt{ne_2^2 \cos^2 \theta + no_2^2 \sin^2 \theta}} \quad (A)$$

In Equation (A), no₂ denotes the ordinary ray refractive index of the second fibers 51, and ne₂ denotes the extraordinary ray refractive index of the second fibers 51, and θ denotes an incident angle of light with respect to the second fibers 51 (length direction).

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The P-polarization component vibrates along a plane parallel to a cross-section of the second fibers 51 in the length direction. Accordingly, the P-polarization component may be influenced by the effective extraordinary ray refractive index ne_{2_eff} of the second fibers 51 in the length direction, but is not influenced by the ordinary ray refractive index no₂ along the cross-sectional direction.

On the other hand, the S-polarization component vibrates along the plane parallel to the cross-section of the second fibers 51. Accordingly, the S-polarization component may be influenced by the ordinary ray refractive index no₂ of the second fibers 51 in the cross-sectional direction but is not influenced by the effective extraordinary ray refractive index ne_{2_eff} of the second fibers 51 in the length direction.

When light is incident from the second supporting medium 52 to the second fibers 51 or from the second fibers 51 to the second supporting medium 52, the P-polarization component is influenced by the effective extraordinary ray refractive index ne_{2_eff} and is refracted or reflected, and the S-polarization component is influenced by the ordinary ray refractive index no₂ and is refracted or reflected. The second fibers 51 are arranged in the light homogenization layer 50 such that the length direction thereof is parallel to the light guide direction. Accordingly, an interface between the second fibers 51 and the second supporting medium 52 does not lie at a right angle to the light guide direction, and when the P-polarization component or the S-polarization component is refracted or reflected in the corresponding interface, angle distribution in the in-plane direction of light varies. In other words, light may be inclined on the right and left sides of the light guide direction. Accordingly, light propagating in the light guide layer 30 is scattered and diffused at various angles, thereby homogenizing the light direction distribution.

Light is refracted and extended only in a horizontal, left and right direction in the light homogenization layer 50, but the angle in a vertical direction does not vary. Accordingly, both of the P- and S-polarization components do not satisfy the total internal reflection condition due to the light homogenization layer 50. For example, light extends in the horizontal, left and right direction in the light homogenization layer 50 so as to remove only spots of an LED, and a refraction angle in the vertical direction in the polarization separation layer 40 varies such that only the S-polarization component may be emitted from the polarization separation layer 40. Accordingly, a desired polarization component may be emitted from the light guide panel, and also light spots of the LED may be removed.

To perform the light homogenizing function, the refractive index nm2 of the second supporting medium 52 may be different from the ordinary ray refractive index no₂ and the extraordinary ray refractive index ne₂ of the second fibers 51.

However, the light homogenization layer 50 may be act more intensely as a homogenization layer of S-polarization.

The ordinary ray refractive index no₂ and the refractive index nm2 of the second supporting medium 52 may have a difference of 0.03 or greater, and for example, 0.05 or greater or 0.1 or greater.

To scatter and diffuse both the S- and P-polarization components with a proper balance, the ordinary ray refractive index no₂ and the extraordinary ray refractive index ne₂ of the second supporting medium 52 and the refractive index nm2 of the second supporting medium 52 may satisfy Equation (1) below:

$$no_2 < nm_2 < ne_2 \quad (1)$$

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In particular, the refractive index nm_2 of the second supporting medium **52** and the effective extraordinary ray refractive index ne_{2_eff} of the second fibers **51** may satisfy Equation (2) below:

$$no_2 < nm_2 < ne_{2_eff} \quad (2)$$

The refractive index nm_2 of the second supporting medium **52** may satisfy Equation (3) below. The refractive index nm_2 of the second supporting medium **52** is smaller than the effective extraordinary ray refractive index ne_{2_eff} of the second fibers **51**, and thus the P-polarization component may be scattered and diffused. Accordingly, the second supporting medium **52** may function as a light homogenization layer that effectively scatters and diffuses both the P- and S-polarization.

$$no_2 < nm_2 < \sqrt{\frac{ne_2^2 \cdot no_2^2 - ne_2^2 \cdot nl^2 + no_2^2 \cdot nl^2 + ne_2^2 - no_2^2}{no_2^2}} \quad (3)$$

In Equation (3), no_2 denotes the ordinary ray refractive index of the second fibers **51**, and ne_2 denotes the extraordinary ray refractive index of the second fibers **51**, and nl denotes the refractive index of the light guide layer **30**.

Equation (3) is derived from Equation (2) and Equation (A) and Equations (B) through (F).

$$\frac{\sin \theta_i}{\sin \theta_1} = \frac{nl}{ni} \approx nl \quad (B)$$

$$\frac{\sin \theta_{in}}{\sin \theta_{out}} = \frac{nm_2}{nl} \quad (C)$$

$$\theta = \frac{\pi}{2} - \theta_{out} \quad (D)$$

$$\theta_1 = \frac{\pi}{2} - \theta_{in} \quad (E)$$

$$ne_{2_eff} = \sqrt{\frac{ne_2^2 \cdot no_2^2 - ne_2^2 \cdot nl^2 + no_2^2 \cdot nl^2 + ne_2^2 - no_2^2}{no_2^2}} \quad (F)$$

In Equations (B) through (F) above, no_2 denotes the ordinary ray refractive index of the second fibers **51**, ne_2 denotes the extraordinary ray refractive index of the second fibers **51**, ni denotes a refractive index of an external medium of the light guide panel **20**, nl denotes a refractive index of the light guide layer **30**, θ_i denotes an incident angle of light incident on the light guide layer **30**, θ_1 denotes a refraction angle of light incident on the light guide layer **30**, θ_{in} denotes an incident angle of light incident on the light homogenization layer **50**, and θ_{out} denotes a refraction angle of light incident on the light homogenization layer **50**. The light guide panel **20** is usually disposed in air, and a refraction index ni of an external medium of the light guide panel **20** is the same as the refractive index of air (=1) and is expressed by Equation (B).

Equation (F) is derived in Equation (A) by substituting nm_2 as $nm_2 = ne_{2_eff}$ and modifying Equation (A) using Equations (B) through (E). Equation (3) is derived from Equation (2) and Equation (F).

If $nm_2 = ne_{2_eff}$, an incident light component ($\theta = \pi/2$) having a maximum angle among P-polarization does not proceed linearly without being refracted or reflected by the second fibers **51** of the light homogenization layer **50**. Accordingly, the light homogenization layer **50** may not perform the function of light homogenization with respect to the same light component. An effective refractive index of light of the inci-

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dent light component, which has an angle smaller than the maximum angle, is close to the ordinary ray refractive index no_2 .

When Equations (B) through (F) are all satisfied, light homogenization with respect to an incident light component incident to the second fibers **51** at all angles θ may be performed.

When nm_2 and the refractive index ne_{2_eff} denoted by Equation (F) have a difference in refraction of 0.03 or greater, the effect of the light homogenization layer of the P-polarization component may be further improved.

As illustrated in FIG. 5, a density of the second fibers **51** disposed on a central line between adjacent light sources **11** may be greater than a density of the second fibers **51** disposed on an axis in a light emitting direction of the light source **11** in the light homogenization layer **50**. A light amount between adjacent light sources **11** may be reduced and dark portions may be likely to be generated in the area **12** near the light sources **11**. Accordingly, by densely arranging the second fibers **51** between the light sources **11**, a light homogenization effect may be further improved.

The first fibers **41** are arranged in the polarization separation layer **40** such that the length direction of the first fibers **41** lies at a right angle to a light guide direction. Accordingly, a cross-section of the first fibers **41** in a diameter direction may be substantially uniform in any position. As the first fibers **41** hardly vary in form in the length direction, when the P- or S-polarization component is refracted or reflected by the first fibers **41**, light is substantially not scattered on both sides of the light guide direction even when seen from the plane. Light is scattered in the plane according to the light guide direction. Angle distribution in the in-plane direction does not vary substantially.

Light may be scattered in the in-plane direction by the second fibers **51** that extend in a direction perpendicular to the incident surface **30a** in the light homogenization layer **50**. Accordingly, light may be scattered in the in-plane direction, which may not be performed by using just a PSSE of the first fibers **41** that extend in parallel to the incident surface **30a**.

If the S-polarization component is emitted only, light at a phase near to the P-polarization component remains in the light guide layer **30**. To also use the remaining light effectively, the phase difference plate **60** is disposed.

In FIG. 1, the phase difference plate **60** is a $\lambda/4$ plate and has a thickness changing phases of light that is incident to the phase difference plate **60** at right angles by 90 degrees. Light that is totally reflected internally in the light guide layer **30** is not incident to the phase difference plate **40** at a right angle, as shown in FIG. 4.

Conversely, although the S-polarization component is sometimes converted into the P-polarization component, since the S-polarization component is selectively emitted to the outside, a ratio of conversion from the P-polarization component to the S-polarization component is high. As such, the remaining light in the light guide layer **30** is also converted to the S-polarization component, and thus, emission efficiency of the S-polarization component may be increased and light usage efficiency may be improved as a result.

The phase difference plate **40** may be used according to a wavelength band. For example, a birefringence sheet formed by drawing a film formed of, for example, PC, polysulfide (PS), PMMA, polyvinyl alcohol, polyamide, polyester, etc. or a support sheet of a liquid crystal polymer orientation layer, or a multi-layer stack structure may be used as the phase difference plate **40**. A sheet formed by arranging the first or second fibers **41** or **51** used in the polarization separation layer **40** or

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the light homogenization layer **50** in a supporting medium may be used as the phase difference plate **40**.

<Second Embodiment>

FIG. **6** is a side view of a surface light source apparatus **1** according to another example embodiment.

In FIG. **4**, the light homogenization layer **50** is below the light guide layer **30**. However, the position of the light homogenization layer **50** may vary. The light homogenization layer **50** may be stacked on the light guide layer **30**. Thus, as in the surface light source apparatus **1** illustrated in FIG. **6**, the light homogenization layer **50** may also be between the light guide layer **30** and the polarization separation layer **40**.

<Third Embodiment>

FIG. **7** is a side view of a surface light source apparatus **1** according to another example embodiment.

In the surface light source apparatus **1** illustrated in FIG. **7**, the light homogenization layer **50** may be on the polarization separation layer **40**.

<Fourth Embodiment>

FIG. **8** is a side view of a surface light source apparatus **1** according to another example embodiment.

Referring to FIG. **4**, the phase difference plate **60** is mounted on a side opposite to the incident surface **30a** of the light guide layer **30**. However, the phase difference plate **60** may be mounted on a principal surface of the light guide layer **30** opposite to a surface on which the polarization separation layer **40** is stacked. Also, the phase difference plate **60** may be mounted on at least one side besides the incident surface **30a** of the light guide layer **30**.

For example, like the surface light source apparatus **1** illustrated in FIG. **8**, the phase difference plate **60** may be disposed on the principal surface of the light guide layer **30** opposite to the surface on which the polarization separation layer **40** is formed, for example, on a lower surface of the light guide layer **30**. However, when the phase difference plate **60** is on the principal surface or the side of the light guide layer **30** that is perpendicular to the light guide direction of light as illustrated in FIG. **8**, the phase difference plate **60** is a λ in plate, and may have a thickness changing a phase of light incident to the phase difference plate **60** by 180 degrees.

Accordingly, when light is refracted or reflected by the polarization separation layer **40** toward the light guide layer **30**, or is incident to the phase difference plate **60** at an acute angle, a phase of light varies by about 180 degrees, and thus the S-polarized light is maintained. Thus, the S-polarized light is reflected by the reflection plate **70**, returns to the light guide layer **30**, and is emitted from the polarization separation layer **40**. Thus, the S-polarized light is emitted, and light of the P-polarization is prevented from being emitted.

As described above, light that propagates in the light guide layer **30** is usually not incident on the phase difference plate **60** at a right angle, and thus is converted from the P-polarization component to the S-polarization component by the λ on phase difference plate **60**.

<Fifth Embodiment>

FIG. **9** is a side view of a surface light source apparatus according to another example embodiment.

The surface light source apparatus illustrated in FIG. **9** includes a polarization separation light homogenization layer **80**.

In the first through fourth example embodiments described above, the polarization separation layer **40** and the light homogenization layer **50** are separately included.

However, as illustrated in FIG. **9**, the surface light source apparatus may include the polarization separation light

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homogenization layer **80** that is formed by integrating the polarization separation layer **40** and the light homogenization layer **50**.

Referring to FIG. **9**, the polarization separation light homogenization layer **80** includes first fibers **81** and second fibers **82**, and a third supporting medium **83** that supports the first and second fibers **81** and **82**. The first fibers **81** extend parallel to the incident surface **30a** of the light guide layer **30**, and the plurality of first fibers **81** are arranged in a direction perpendicular to the incident surface **30a**. The second fibers **82** extend in a direction perpendicular to the incident surface **30a**, and the plurality of second fibers **82** are arranged in a direction parallel to the incident surface **30a**. For example, the first fibers **81** and the second fibers **82** extend and are arranged in directions at right angles to each other, and while the first and second fibers **81** and **82** are woven with each other, they are supported by the third supporting medium **83**.

In the polarization separation light homogenization layer **80**, an ordinary ray refractive index n_{o1} and an extraordinary ray refractive index n_{e1} of the first fibers **81**, an ordinary ray refractive index n_{o2} and an extraordinary ray refractive index n_{e2} of the second fibers **82**, and a refractive index $n_{matrix3}$ of the third supporting medium **83** satisfy Equations (4) and (5) below:

$$n_{o1} = n_{matrix3} < n_{e1} \quad (4)$$

$$n_{o2} < n_{matrix3} = n_{e2} \quad (5)$$

Accordingly, the first fibers **81** (warp threads) selectively scatter only an S-polarization component and emit the same through a light emitting surface that is an upper surface of the polarization separation light homogenization layer **80**. The second fibers **82** (woof) diffuse light propagating in the light guide layer **30** in an in-plane direction to homogenize a light direction distribution. A refractive index $n_{matrix3}$ of the third supporting medium **83** may correspond to the ordinary ray refractive index n_{o1} of the first fibers **81** and may be different from the extraordinary ray refractive index n_{e1} of the first fibers **81**. Thus, the P-polarization component may not be refracted by the first fibers **81** but proceed straight, and only the S-polarization component may be influenced by the extraordinary ray refractive index n_{e1} of the first fibers **81** and a portion thereof may be emitted through the light emitting surface.

On the other hand, the refractive index $n_{matrix3}$ of the third supporting medium **83** may be different from the ordinary ray refractive index n_{o2} and the extraordinary ray refractive index n_{e2} of the second fibers **82**. Accordingly, the S-polarization component may not be refracted by the second fibers **82** but proceed straight, and only the P-polarization component may be influenced by the extraordinary ray refractive index n_{e1} of the second fibers **82** and be refracted and reflected to be diffused in the in-plane direction.

As the first and second fibers **81** and **82**, the first and second fibers **41** and **51** described above may be used, and the first supporting medium **42** or the second supporting medium **52** may be used as the third supporting medium **83**. However, in an example embodiment, in order to satisfy Equations (4) and (5), the first fibers **81** and the second fibers **82** may be formed of different materials.

<Sixth Embodiment>

FIG. **10** is a side view of a surface light source apparatus **1** according to another example embodiment.

In the first through fifth embodiments (FIGS. **1** through **9**), the light guide layer **30** is formed of a material different from the first supporting medium **42** and the second supporting medium **52**.

However, the light guide layer **30** may be formed of the same material as a material of at least one of the first supporting medium **42** and the second supporting medium **52**.

A light guide layer **34** in the surface light source apparatus **1** illustrated in FIG. **10** corresponds to the light guide layer **30** of the surface light source apparatus **1** of FIG. **1** and is formed of the same material as the first supporting medium **42**. For example, the light guide layer **34** may be regarded as the light guide layer **30** and the polarization separation layer **40** according to the example embodiment of FIG. **1** integrated into a single layer.

Although not shown in the drawings, the light guide layer **30** of the surface light source apparatus **1** may be formed of the same material as the second supporting medium **52** so that the light guide layer **30** and the light homogenization layer **50** are integrated into a single layer. Although not shown in the drawings, in the surface light source apparatus **1** of FIG. **1**, the light guide layer **30**, the first supporting medium **42**, and the second supporting medium **52** may all be formed of the same material so that the light guide layer **30**, the polarization separation layer **40**, and the light homogenization layer **50** are integrated into a single layer.

In the surface light source apparatus of FIG. **9**, in which the polarization separation light homogenization layer **80** is formed by integrating the polarization separation layer **40** and the light homogenization layer **50**, the light guide layer **30** may be formed of the same material as the third supporting medium **83** to integrate the polarization separation light homogenization layer **80** and the light guide layer **30** into a single layer.

By integrating the light guide layer **30** with the polarization separation layer **40** and/or the light homogenization layer **50**, manufacturing may be simplified and manufacturing costs may be reduced, and both a light guide panel and a surface light source apparatus having a thin thickness may be manufactured.

The first fibers **41** are arranged in an upper portion of the light guide layer **34** of FIG. **10**. Alternatively, the first fibers **41** may be arranged throughout light guide layer **34**, or in an area different from the upper portion of the light guide layer **34**.

<Seventh Embodiment>

FIG. **11** is a side view of a surface light source apparatus **1** according to another example embodiment.

In the surface light source apparatus **1** according to the first through sixth example embodiments, the light source unit **10** is on a side along a short-axis of the light guide layer **30** constituting the light guide panel **20**.

However, the surface light source apparatus **1** may include a plurality of light source units **10**. For example, as illustrated in FIG. **11**, the light source units **10** may be disposed on both sides along the short-axis of the light guide layer **30**.

The surface light source apparatus **1** illustrated in FIG. **11** corresponds to the surface light source apparatus **1** of FIG. **8**, except that the light source units **10** are on a side of the surface light source apparatus **1** illustrated in FIG. **11** instead of the reflection plate **70**.

Although not shown in the drawings, in some of the above-described example embodiments, for example, in the surface light source apparatuses **1** of the first, second, and fourth embodiments, the light source units **10** may be disposed on both sides along the short-axis of the light guide layer **30**. For example, the light source units **10** may face each other with respect to the light guide layer **30**.

The light source units **10** may be further disposed on a side besides a light-emitting surface of a long-axis of the light guide layer **30**.

EXPERIMENTAL EXAMPLES

Experimental examples conducted to verify the effects of the surface light source apparatuses according to some example embodiments and a comparative example are described. The technical scope is not limited to the experimental examples.

Experimental Example 1

Preparation of Light Guide Layer

As a light guide layer, PMMA (size: 6 cm×9 cm) was prepared.

(2) Formation of Polarization Separation Layer

As a first fiber, PET fibers (material: PET, $n_o=1.5449$, $n_e=1.7200$, a surface roughness of external circumferential surface (R_z)= $2\text{ }\mu\text{m}$, cross-section: circular (diameter: $20\text{ }\mu\text{m}$)) were arranged to a thickness of fifteen layers in one direction on an upper surface of the prepared light guide layer. As a first supporting medium designed to have a refractive index of 1.545 after curing, a UV curable resin was penetrated between the PET fibers. A mixture of 40 parts by weight of EA-F5503 available by Osaka Gas Chemicals Co., Ltd.; 58 parts by weight of MK esterA-400 available by Shin Nakamura Chemical Co., Ltd.; and 2 parts by weight of Photopolymer Initiator Irgacure available by Shiba Specialty Chemicals was used as the UV curable resin. The air between the PET fiber and the UV curable resin was removed by vacuum degassing, and then the UV curable resin was covered with a released glass plate, and a UV lamp was used to cure the UV curable resin. The glass plate was exfoliated to form a polarization separation layer on the light guide layer.

When observing a cross-section of the polarization separation layer using a laser microscope (available by Keyence Corporation VK-9600), as illustrated in FIG. **11**, the polarization separation layer has a structure in which the first fibers arranged in one direction are supported by the UV curable resin.

(3) Formation of Light Homogenization Layer

As a second fiber, N610 fibers (material: Nylon 6,10, $n_o=1.5217$, $n_e=1.5711$, cross-section: circular (diameter: $50\text{ }\mu\text{m}$)) were arranged on a lower surface of the prepared light guide layer in three layers in a direction perpendicular to the arrangement direction of the first fibers of the polarization separation layer. As a second supporting medium designed to have a refractive index of 1.571, a UV curable resin was penetrated between the N610 fibers. A mixture of 40 parts by weight of EA-F5503 available by Osaka Gas Chemicals Co., Ltd.; 58 parts by weight of MK esterA-400 available by Shin Nakamura Chemical Co., Ltd., and 2 parts by weight of Photopolymer initiator Irgacure available by Shiba Specialty Chemicals may be used as the UV curable resin. By curing the UV curable resin in the same manner as when forming the polarization separation layer, a light homogenization layer was formed on the light guide layer.

(4) Arrangement of Light Source Unit, Phase Difference Plate, and Reflection Plate

A light source unit including nine LEDs as light sources arranged in one dimension (serial arrangement) is installed along a short-axis of the light guide layer. The side at which the light source unit is installed is set to be parallel to the length direction of the first fibers of the polarization separation layer, and perpendicularly to the length direction of the second fibers of the light homogenization layer, and the arrangement direction of the LEDs is set to be in a direction parallel to the length direction of the first fibers of the polarization separation layer. Then, a $\lambda/2$ phase difference plate is

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arranged at a side of the light guide layer opposite to the side where the light source unit is installed. Also, a reflection plate is mounted on all surfaces except an upper surface of the polarization separation layer (light-emitting surface) and the side on which the light source unit is installed. Consequently, the surface light source apparatus was manufactured. The surface light source apparatus according to Experimental example 1 corresponds to the surface light source apparatus of the example embodiment illustrated in FIG. 1.

Experimental Example 2

A light homogenization layer was formed on the upper surface of the light guide layer. The surface light source apparatus was manufactured in the same manner as Experimental example 1 except that PET fibers (PET, $n_o=1.5449$, $n_e=1.7200$, a surface roughness of external circumferential surface (R_z)= $2\text{ }\mu\text{m}$, cross-section: circular (diameter: $20\text{ }\mu\text{m}$)) were used as the second fiber, and a UV curable resin designed to have a refractive index of 1.605 after curing was used as the second supporting medium. A mixture of 68 parts by weight of EA-F5503 available by Osaka Gas Chemicals Co., Ltd.; 30 parts by weight of benzylacrylate; and 2 parts by weight of Photopolymer Initiator Irgacure 184 available by Shiba Specialty Chemicals may be used as the UV curable resin.

The surface light source apparatus manufactured according to Experimental example 2 corresponds to the surface light source apparatus 1 illustrated in FIG. 6.

Experimental Example 3

A polarization separation layer was formed on the upper surface of a light guide layer. Except that a light homogenization layer was formed on the upper surface of the polarization separation layer, the surface light source apparatus was manufactured in the same manner as Experimental example 2.

The surface light source apparatus manufactured in Experimental example 3 corresponds to the surface light source apparatus 1 illustrated in FIG. 7.

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Experimental Example 4

A surface light source apparatus was manufactured in the same manner as Experimental example 2 except that PET fibers (PET, $n_o=1.5449$, $n_e=1.7200$, a surface roughness of external circumferential surface (R_z)= $2\text{ }\mu\text{m}$, cross-section: equilateral triangular (each side length: $10\text{ }\mu\text{m}$)) were used as first fibers forming the polarization separation layer.

Comparative Example 1

A surface light source apparatus was manufactured in the same manner as Experimental example 1 except that a light homogenization layer was not formed.

[Evaluation]

In the surface light source apparatuses obtained in the experimental examples and Comparative example 1, a luminance of light emitted from the light emitting surface and luminance spots and a polarization of the light were measured. The luminance, the luminance spots, and the polarization were measured by using a two-dimensional colorimeter, Konica Minolta CA-2000 or Conoscope 80 available by AUTRONIC-MELCHERS GmbH in combination with a polarization plate to calculate a ratio of a desired polarization component. A luminance was measured by driving the serially-arranged nine LEDs with a constant current of 30 mA. As the luminance of emitted light, front luminance in the center of the light-emitting surface of the light guide panel was measured. Table 2 below shows the measurement result.

Referring to FIGS. 13 and 14, two-dimensional luminance distribution of light emitted from an upper surface of the light guide panel (light-emitting surface) of the surface light source apparatuses manufactured according to Experimental example 2 and Comparative example 1 measured by CA-2000 is shown. The same two-dimensional luminance distribution as that shown in FIG. 13 may be obtained from the surface light source apparatuses manufactured according to Experimental examples 1, 3, and 4.

TABLE 2

	Stacking order of light homogenization layer, light guide layer, and polarization separation layer	polarization		light homogenization		Evaluation		
		separation layer		layer		Luminance spots	Luminance ($\text{cd}/\text{m}^2\text{m}^2$)	Polarization (s polarization:p polarization)
		First fiber	First supporting medium	Second fiber	Second supporting medium			
Experimental Example 1	Light homogenization layer, light guide layer, polarization separation layer	$n_o = 1.545$ $n_e = 1.720$	$n_{m1} = 1.545$	$n_o = 1.5217$ $n_e = 1.5711$	$n_{m2} = 1.571$	No stripe spots in light	1200	16:1
Experimental Example 2	Light guide layer, light homogenization layer, polarization separation layer	$n_o = 1.545$ $n_e = 1.720$	$n_{m1} = 1.545$	$n_o = 1.545$ $n_e = 1.720$	$n_{m2} = 1.605$	No stripe spots in light	1400	15:1

TABLE 2-continued

	Stacking order of light homogenization layer, light guide layer, and polarization separation layer	polarization		light homogenization		Evaluation		
		separation layer		layer		Luminance spots	Luminance (cd/m ² m ²)	Polarization (s polarization:p polarization)
		First fiber	First supporting medium	Second fiber	Second supporting medium			
Experimental Example 3	Light guide layer, polarization separation layer, light homogenization layer	no = 1.545 ne = 1.720	nm ₁ = 1.545	no = 1.545 ne = 1.720	nm ₂ = 1.605	No stripe spots in light	1300	10:1
Experimental Example 4	Light guide layer, light homogenization layer, polarization separation layer	no = 1.545 ne = 1.720	nm ₁ = 1.545	no = 1.545 ne = 1.720	nm ₂ = 1.605	No stripe spots in light	2900	15:1
Comparative example 1	Light guide layer, polarization separation layer	no = 1.545 ne = 1.720	nm ₁ = 1.545	—	—	No stripe spots in light	1000	16:1

In the surface light source apparatuses of Experimental examples 1 through 4 in which the light homogenization layer is included, as illustrated in FIG. 13, stripe spots are not observed in light emitted from the upper surface of the stacked structure. Thus, as can be seen from this result, according to the surface light source apparatuses of some of the example embodiments, luminance spots are removed when an LED, which is a discontinuous light source, is used. According to the surface light source apparatuses manufactured according to the above experimental examples, high polarization separation performance may be obtained.

In the surface light source apparatus manufactured according to Comparative example 1, a ratio of polarization separation is similar to that of Experimental examples. However, as illustrated in FIG. 14, stripe spots are clearly observed in light emitted from the upper surface of the stacked structure.

In the surface light source apparatus of Experimental example 4 in which the first fibers of the polarization separation layer have an equilateral triangular cross-section, an intensity (luminance) of light emitted in a direction perpendicular to the light guide layer (light emitted from the upper surface of the stacked structure) is twice as large as that in the surface light source apparatus of Experimental example 2 in which the first fibers have a circular cross-section.

As described above, according to at least one of the example embodiments, the surface light source apparatuses have excellent polarization separation performance, and, even when a discontinuous light source such as an LED is used, stripe spots of light may be prevented.

Hereinafter, a flat panel display according to an example embodiment will be described.

The flat panel display includes a liquid crystal panel on which an image is formed and a light source apparatus that supplies light used in displaying the image to the liquid crystal panel. The light source apparatus may be a surface light source apparatus according to the example embodiments. The liquid crystal panel may be on a surface from which light of

the surface light source apparatus is emitted. The liquid crystal panel may be a typical liquid crystal panel.

It should be understood that the example embodiments described herein should be considered in a descriptive sense only and not for purposes of limitation. Descriptions of features or aspects within each example embodiment should typically be considered as available for other similar features or aspects in other example embodiments.

What is claimed is:

1. A light guide panel comprising:

a light guide layer having a light incident surface;

a polarization separation layer configured to select a desired polarization among light emitted from the light guide layer and to emit light having the desired polarization; and

a light homogenization layer including a plurality of first fibers and a first supporting medium of the first fibers, the light homogenization layer configured to diffuse and scatter light incident on the light incident surface into the light guide layer.

2. The light guide panel of claim 1, wherein the polarization separation layer comprises:

a plurality of second fibers having birefringence; and
a second supporting medium that is isotropic and configured to support the second fibers.

3. The light guide panel of claim 2, wherein a refractive index of the second supporting medium corresponds to at least one of two different refractive indices of the second fibers.

4. The light guide panel of claim 1, wherein the polarization separation layer comprises:

a plurality of second fibers having birefringence; and
a second supporting medium that is isotropic and configured to support the second fibers; and
wherein the plurality of first fibers have birefringence, and the first supporting medium is isotropic and configured to support the first fibers.

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5. The light guide panel of claim 4, wherein a refractive index of the first supporting medium is different from at least one of the two different refractive indices of the first fibers.

6. The light guide panel of claim 4, wherein an ordinary ray refractive index n_{o2} and an extraordinary ray refractive index n_{e2} of the first fibers and a refractive index n_{m2} of the first supporting medium satisfy Equation (1) below:

$$n_{o2} < n_{m2} < n_{e2} \quad (1).$$

7. The light guide panel of claim 2, wherein a surface roughness R_z of an outer circumferential surface of the second fibers is from about 0.1 μm to about 10 μm .

8. The light guide panel of claim 2, wherein the second fibers have a polygonal cross-section in a radius direction.

9. The light guide panel of claim 4, wherein one of the light guide layer, the polarization separation layer, and the light homogenization layer is between the remaining two layers.

10. The light guide panel of claim 2, further comprising:
a phase difference plate configured to convert a polarization direction of light in the light guide layer; and
a reflection plate on a surface other than (i) the light incident surface and (ii) a light emitting surface of the light guide layer, the reflection plate configured to reflect light emitted from the light guide layer back into the light guide layer.

11. The light guide panel of claim 9, wherein the polarization separation layer and the light homogenization layer are on the light emitting surface of the light guide layer.

12. The light guide panel of claim 11, wherein the polarization separation layer and the light homogenization layer are integrated into a single layer.

13. The light guide panel of claim 12, wherein in the single layer, the first fibers and the second fibers alternate, and a third supporting medium includes the first and second supporting media and is configured to support the first and second fibers.

14. The light guide panel of claim 12, further comprising:
a phase difference plate configured to convert a polarization direction of light in the light guide layer; and
a reflection plate on a surface other than (i) the light incident surface and (ii) the light emitting surface of the light guide layer, the reflection plate configured to reflect light emitted from the light guide layer back into the light guide layer.

15. The light guide panel of claim 9, wherein the light guide layer is a same material as at least one of the first and second supporting media.

16. The light guide panel of claim 13, wherein an ordinary ray refractive index n_{o1} and an extraordinary ray refractive index n_{e1} of the second fibers, an ordinary ray refractive index n_{o2} and an extraordinary ray refractive index n_{e2} of the first fibers and a refractive index $n_{matrix3}$ of the third supporting medium satisfy Equations (4) and (5) below:

$$n_{o1} = n_{matrix3} < n_{e1} \quad (4)$$

$$n_{o2} < n_{matrix3} = n_{e2} \quad (5).$$

17. The light guide panel of claim 4, wherein a density of the second fibers is higher away from the light incident surface.

18. The light guide panel of claim 4, wherein a density of the first fibers varies according to arrangement positions.

19. The light guide panel of claim 4, wherein some of the plurality of first and second fibers comprise discontinuous portions.

20. The light guide panel of claim 4, wherein portions of the plurality of first and second fibers overlap.

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21. The light guide panel of claim 13, wherein the first fibers and the second fibers are different materials.

22. A surface light source apparatus comprising:

a light source unit including a plurality of light sources spaced apart from one another; and

a light guide panel configured to emit light having a polarization component of light incident from the light source unit,

wherein the light guide panel is one of claim 1.

23. The surface light source apparatus of claim 22, wherein the polarization separation layer comprises:

a plurality of second fibers having birefringence; and

a second supporting medium that is isotropic and configured to support the second fibers; and

wherein the plurality of first fibers have birefringence, and the first supporting medium is isotropic and configured to support the first fibers.

24. The surface light source apparatus of claim 23, wherein a density of the first fibers is higher between the plurality of light sources.

25. The surface light source apparatus of claim 22, wherein the plurality of light sources are on two opposite sides of the light guide panel.

26. The surface light source apparatus of claim 23, wherein one of the light guide layer, the polarization separation layer, and the light homogenization layer is between the remaining two layers.

27. The surface light source apparatus of claim 23, further comprising:

a phase difference plate configured to convert a polarization direction of light in the light guide layer; and

a reflection plate on a surface except (i) the light incident surface and (ii) a light emitting surface of the light guide layer, the reflection plate configured to reflect light emitted from the light guide layer back into the light guide layer.

28. The surface light source apparatus of claim 26, wherein the polarization separation layer and the light homogenization layer are on the light emitting surface of the light guide layer.

29. The surface light source apparatus of claim 23, wherein the polarization separation layer and the light homogenization layer are integrated as a single layer.

30. The surface light source apparatus of claim 29, wherein in the single layer, the first fibers and the second fibers alternate, and a third supporting medium includes the first and second supporting media and is configured to support the first and second fibers.

31. The surface light source apparatus of claim 29, further comprising:

a phase difference plate configured to convert a polarization direction of light in the light guide layer; and

a reflection plate on a surface except (i) the light incident surface and (ii) a light emitting surface of the light guide layer, the reflection plate configured to reflect light emitted from the light guide layer back into the light guide layer.

32. The surface light source apparatus of claim 26, wherein the light guide layer is a same material as at least one of the first and second supporting media.

33. The surface light source apparatus of claim 23, wherein a density of the second fibers is higher away from the light incident surface.

34. A flat panel display comprising:

a light source apparatus; and

a liquid crystal panel configured to display an image with light supplied from the light source apparatus,

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wherein the light source apparatus is the surface light source apparatus of claim 22.

35. The flat panel display of claim 34, wherein the plurality of first fibers have birefringence and the first supporting medium is isotropic and configured to support the first fibers.

36. The light guide panel of claim 1, wherein the light homogenization layer is provided in a lengthwise direction of the light guide layer.

37. The light guide panel of claim 36, wherein the light homogenization layer is provided substantially over an entire portion of a surface of the light guide layer.

38. The device of claim 14, wherein the light homogenization layer is provided one of in a first direction perpendicular to the light incident surface and in a second direction which is inclined by about $\pm 45^\circ$ with respect to the first direction perpendicular to the incident surface .

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